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Catia customization for Design and Modeling of Two stage spur Gearbox

Mayuresh V. Patwardhan
<u>mayuresh.patwardhan26@gmail.com</u>
Rajarambapu Institute of Technology, Sakharale,
Maharashtra

Uddhavrao Nimbalkar <u>uddhavrao.nimbalkar@ritindia.edu</u> Rajarambapu Institute of Technology, Sakharale, Maharashtra

ABSTRACT

In this paper, we describe how the customization of design task, in solid modeling with CATIA V5 for two stage spur gearbox can be approached, by means of macros (piece of code) and with GUI form. The user has to supply some basic requirements of the gearbox and rest of the different parameters for design of gearbox is calculated by formulas. And then with the help of these parameters, part model of gearbox is created.

Keywords— CAD, Catia, GUI, Macros, Design, Parametric modeling, two stage spur gearbox

1. INTRODUCTION

Current scenario of the market is competitive. To sustain in the market for company product time to the market have to be minimum. Companies existing product demands from the customer are to be provided quickly as soon as possible. Existing product requirement has same parametric features of components for different specification. Design and modeling time of the product is generally 60-70% of overall time of the product development. Design phase has lot of potential where time can be saved. Parametric modeling can be used for saving the modeling time. Knowledge based approach can be useful for saving the design time. Lot of repetitive calculations can be saving for avoiding tedious work. CATIA software is selected having strong parameterization. Mechanical product selected is gearbox. Nowadays best of the best innovations are coming into picture, in these, researchers have made one way to reduce maximum design time by doing design automation concept which means integration of GUI developed with the help of computer programming language and market available CAD packages. Graphical User Interface (GUI) is the only way for users to communicate with the system.

But no specific software is available for the design of a specific product. So by this dissertation approach it is very important to make one tailor-made software which will be useful for complete design of a specific component and output of the software should easily be integrated with other modeling software. In this with use of Macro which means program written for specific task. For developing advanced macros for special needs Catia V5 is an open system. Macros may be useful for creating, analyzing, measuring, modifying. Translating, optimizing surfaces, solids, wireframes and more. Macros are useful for part operation, assembly operation and all multidisciplinary applications.

2. LITERATURE REVIEW

Many research attempts have been made in the area of parametric modeling.

Ruchik D. Trivedi et al [1] discussed about integrating the commercially available package Pro/E with Microsoft Excel spreadsheet for 3D parametric modeling. Various product variants of the inner ring of spherical roller bearing have been executed by parametric designing concept in Pro/Engineer Wildfire.

Umesh Bedse et al [2] discussed about developed GUI is made for the case study of design of CI engine parts like cylinder head, cylinder block, piston and crankshaft. CI engine is having many numbers of mechanical components, but parts named above are the most important parts of any CI engine. So design of these parts is useful to take into account to develop a GUI. And Creo software is used for modeling.

Indrajitsinh J. Jadeja et al [3] discussed about the work reviews the procedural steps involved in the design of couplings and the development of the software package using visual basic as a tool for the design. This system is carried out on the case study of flange coupling and standard design equation being carried out together with the use of programming software and use CREO as modeling software.

Dhaval b. shah et al [4] discussed about the 3D models for flange type coupling and related dimension database in Microsoft Excel have been prepared. This Excel sheet has been linked with Autodesk Inventor to transfer data and relate to respective features of the part. User can update the model just by modifying the sheet. This takes comparatively very less time to generate complex part models with respect to generating them individually. This automation can further be proceeded by exporting models to the analysis or CAM package.

L. Karikalan et al [5] discussed about the main purpose of this assignment is to provide a gear box with Low reduction ratio, low weight and efficient for engine up to 500cc. It should also be used in "All Terrain" vehicles.

3. CATIA V5

CATIA (Computer Aided Three Dimensional Interactive Application) is a multi-platform CAD/CAM/CAE commercial software suite developed by French company Dassault Systems and it is marketed world-wide by IBM. Catia is the world's leading CAD/CAM/CAE software. For developing advanced macros for special needs Catia V5 is open system. A macro is a series of functions, written in a scripting language, that you group in a single command to perform the requested task automatically. These macros may be useful for creating, analyzing, measuring, modifying. Translating, optimizing surfaces, solids, wireframes and more. Macros are used to save time, reduce the possibility of human error by automating repetitive processes, standardization, improving efficiency, expanding Catia's capabilities, and for streamlining tasks. For creating basic structure and basic flow of program we require inputs, outputs, and supporting data from the user. Catia provides customization capability. In Catia the part Objects, which are used for developing part model i.e. three dimensional object are structured under a automation tree.

4. CATIA V5 MACROS

A macro is a series of functions, written in a scripting language, that you group in a single command to perform the requested task automatically. In simple it is a piece of code written in certain programming language which groups a set of operation that defines a certain task. For each task separate code is written and assembled together by using forms.

4.1 CATIA Customization/Automation Objects

In CATIA the part objects, which are used for developing part model i.e. three dimensional object are structured under a tree as shown in the following figure. As and when needed the part object can be extracted with the macro programming for customization or automation of CATIA V5 The Part Document object aggregates, or includes, the part tree structure starting with the Part object located at the top of the part specification tree. These Part Document objects are: Origin Element, Geometric Elements, Bodies and Part objects are: Constraints, Relations, Parameters, and Factory3D, Shape Factory (Sketches, Geometric Elements, and Shapes)

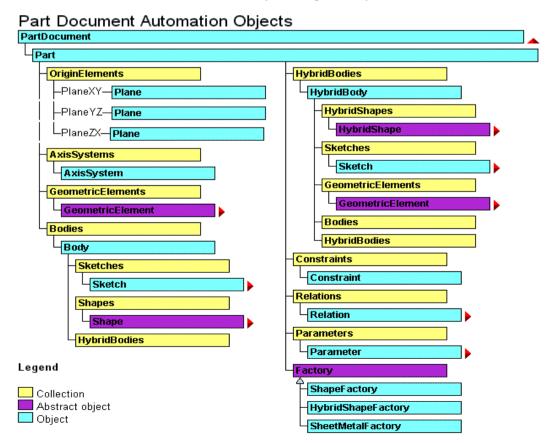


Fig 1: Part Modeling Object Tree

5. METHODOLOGY

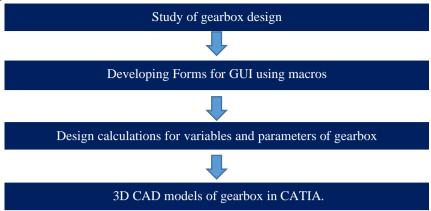


Figure 2: Methodology

1. First user need to give input parameters of gearbox to GUI form

The input parameters are as follows

Power (P) in KW No. of teeth on gear 1 (Z1) service factor

- \Rightarrow RPM of Gear 1 (N1) \Rightarrow No. of teeth on gear 3 (Z3) \Rightarrow factor of safety
- ⇒ RPM of Gear 4 (N4) ⇒ surface hardness (BHN) ⇒ Ultimate stress for gear material Sut N/mm²
- 2. As the input parameters are given from calculate module we get the value which is best suitable according to design procedure of gearbox
- 3. As user fill that value into the input module value the design is getting checked
- 4. And gear dimensions are generated and model is generated.

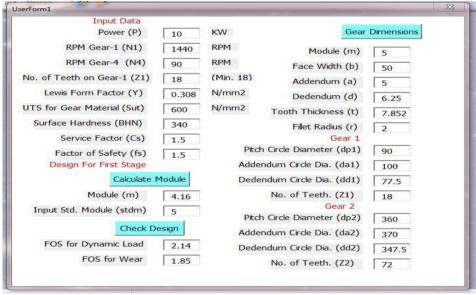


Figure 3: Developed GUI

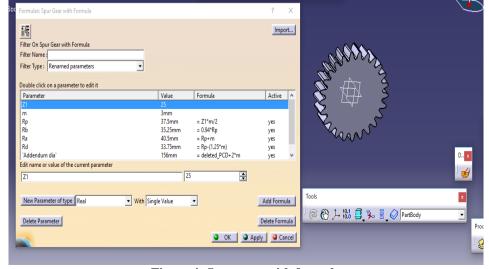


Figure 4: Spur gear with formula

Design calculations

Desi	gn calculations				
		Notat	Value	I Init	Eamoula
	Toward Dada	ion	Value	Unit	Formula
	Input Data	ъ	10	17337	
	Power to be transmitted	P	10	KW	
	RPM of Input Shaft (Gear 1)	N1	1440	RPM	
	RPM of Output Shaft (Gear 4)	N4	90	RPM Min 18 for	r 20 Degree
	Minimum number of teeth for Gear 1	Z 1	18	Pressure a	
	Lewis form Factor for Gear 1	Y1	0.308		
				N/mm2,	
	UTS of Gear material	Sut	600	Mpa	
	Surface Hardness for Gears	BHN	340	Maximum	torque or
	Service factor	Cs	1.5		rque /Rated torque
	Factor of Safety	fs	1.5	υ	
	•				
	Assumptions				
	Gear teeth pressure angle		20		
	Pitch line velocity	v	5	m/s	
	·				b - Width of gear, m-
	Ratio b/m	b/m	10		module
	Material for all gears is considered same, the pinion is weaker than gear,				
	Hence it is necessary to design for Pinion i.e.				
	Gear 1				
A	Module Based on Beam Strength				
	Velocity Factor	Cv	0.375		3/(3+v)
	Permissible bending stress for gear teeth	□b	200	N/mm2	Sut/3
	Terminolog condaing outers for genit teetin		66305.9	1 1/ 111112	
	Torque transmitted by Gear 1	Mt	6223	Nmm	(60*10^6)*(P)/(2*3.142*N1)
			1909611		
	Module step-1		7		60*10^6/3.142
	Module step-2		22.50		P*Cs*fs
	•		5987520		
	Module step-3		.000		Z1*N1*Cv*(b/m)*b*Y
	Module step-4		71.760		Step1*(step2/step3)
	Module Based on Beam Strength	m'	4.16		Cuberoot(step-4)
В	Selection of Module & FOS For Beam Strength	& Wear	r Strength		
_	Standardized Module	stdm	5		
	Pitch Circle diameter for Gear 1	dp1	90	mm	m*Z1
	Then choic diameter for deal 1	ч	70		21
В					
1	FOS For Considering Dynamic load		1472 46		
	Tangential force due to rated torque	Pt	1473.46 5827	N	
	Actual Pitch line velocity	Va	6.78672	m/s	Create If Function for Cv
	Velocity Factor	Cv	0.30654	114 0	Cleane II I uniculon 101 CV
	. 0.0011, 1 40101	٠v	7210.19		
	Effective load	Peff	87		Peff=Cs*Pt/Cv
	Beam Strength	Sb	15400.0 00	N	m*b**sb*Y
	FOS Considering Dynamic load	Sb Fsb	2.1359	1.4	m·u·su·1
	105 Considering Dynamic toad	1.20	4.1337		

FOS For Wear or Pitting Failure

Total transmission ratio	i	16		N1/N4	
Speed reduction at each stage	i1	4.000		sqrt(i)	
	Z2'	72.000		i1*Z1	
Number of teeth for Gear 2	$\mathbb{Z}2$	72			
Pitch Circle diameter for Gear 2	dp2	360	mm		
Width of gear tooth	b	50	mm		
Ratio factor for external gears	Q	1.6000		Q = 2Z2/(Z1+Z2)	
Load stress factor	K	1.8496		K=0.16*(BHN/100)^2	
		13317.1			
Wear strength for Gear	Sw	2000	N	Sw = b*Q*dp1*K	
FOS for wear load	Fsw	1.84698		Fsw=Sw/Peff	

IF Fsw is less than 1, Message Box Increase Module

IF Fsw is more than 1, Message Box Design is safe against wear load

Gear Dimensions						E.g.
				(b/m)*	tbmg	tb- template box for
Module	m	5	mm	m	-	mg
T		7 0				tb- template box for
Face Width	b	50	mm	m	tbb	b value
Addendum	a	5	mm	m 1.25*	tba	
Dedendum	d	6.25	mm	m	tbd	
Tooth Thickness	t	7.854	mm	1.5708 *m	tbt	
			mm			
Fillet radius	r	2	mm	0.4*m	tbr	
Gear 1						
					tbdp1	
Pitch Circle diameter	dp1	90	mm		g	
				dp1+2		
Addendum Circle diameter	da1	100	mm	*a	tbda1	
	1.11	77.5		dp1-	.1 111	
Dedendum Circle Diameter	dd1	77.5	mm	2*d	tbdd1	
Number of teeth	Z 1	18			tbZ1g	
Gear 2						
					tbdp2	
Pitch Circle diameter	dp2	360	mm		g	
				dp1+2		
Addendum Circle diameter	da2	370	mm	*a	tbda2	
				dp1-		
Dedendum Circle Diameter	dd2	347.5	mm	2*d	tbdd2	
Number of teeth	Z 2	72			tbZ2g	

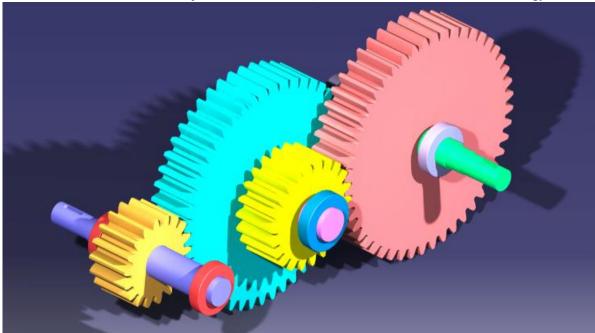


Figure 5: Model for assembly of gearbox

D Shaft Selection Shaft 1 Center Distance between Gear1 &				
Gear2	C1	225	mm	(dp1+dp2)/2
Center Distance between Gear3 & Gear4	C2	225	mm	(dp3+dp4)/2
ASME code for Bending moment	kb	1.5		
ASME code for torsional moment	kt	1		
Assumptions				
Factor of Safety for shaft 1	Fss	2		
Distance Between Bearings on Shaft 1	L1	200	mm	
Permissible Shear Stress	Ssy	108	N/mm2	0.18*Sut
Gears are fixed on shaft by Keyways, Therefore	tmax	40.5	N/mm2	0.75*Ssy/Fss
Tangential Force at Gear 1 (C)	Ftc	1473.466	N	T1x2/dp1
Axial Force at Gear 1	Fac	536.298	N	Ftc* tan20
Resultant force at C	Fct	1568.030	N	Ftc/ Cos20 3.142/4*dp1*dp1*b* (7.85*10^(-
Weight of Spur Gear 1	Ws1	24.499	N	6))*9.81
Total Resultant Force at C	Fc	1592.528		
Reactions at A	Ra	796.264	N	Fc*(L1/2)/L1
Reactions at B	Rb	796.264	N	Fc-Ra
Maximum Bending moment at C	Mbc	79626.40518	Nmm	Fc*L1/4
Equivalent twisting moment	Te1	136610.0309		$Sqrt((Kb*Mbc)^2+(Kt*Mt)^2)$
Shaft 1 Diameter cube	d1^3	17176.76477		(16/(3.142*tmax))*Te
Shaft 1 Diameter	d1	25.802		

25.00 mm

27.00 mm

Shaft 2

Considering next standard value for Shaft Diameter

Distance Between Bearings on Shaft 2	L2	180	mm	
Distance Between Bearing and Spur Gear 2	LEG	45	mm	
Distance Between Gear 2 & 3	LGH	90	mm	
	LEH	135		
	LHF	45		
Tangential Force at Gear 2 (G)	FtG	368.366	N	Mt/(dp2/2)
Weight of Gear 2	Wg2	389.9790136		1
Total force at Gear 2	FG	758.345	N	
Tangential Force at Gear 3 (H)	FtH	1473.466	N	Mt/(dp3/2)
Weight of Gear 3	Wg3	24.37369	N	
Total force at Gear 3	FH	1497.840		
Talina manual of E. Ermand E.	DE	1212 066004	NI	(FG*LEG+
Taking moment at E, Force at F	RF	1312.966004	N	(FH*(LEG+LGH)))/L2
Force at E	RE	943.219	N	FG+FH-RF
Bending moment at G	MG	42444.85418	Nmm	RE*LEG
Bending moment at F	MH	59083.4702	Nmm	RE*LEH-FG*LGH
Bending moment at 1	14111	37003.1702	1 111111	RE LETT'S LOT
Maximum Bending moment	Mmax2	59083.4702	Nmm	
Equivalent Twisting moment	Te2	110683.8183	Nmm	$Sqrt((Kb*Mmax2)^2+(Kt*T)^2)$
	d2^3	13916.91298		
	d2	24.05364907	mm	
		24	mm	
Considering next standard value for				
Shaft Diameter	d2	26	mm	
Shaft Diameter	d2	26	mm	
Shaft Diameter Shaft 3	d2 L3	26240	mm	
Shaft Diameter Shaft 3 Distance Between Bearings on Shaft 3 Distance Between Bearing and Spur	L3	240		
Shaft Diameter Shaft 3 Distance Between Bearings on Shaft 3	L3 LKJ	240 150		
Shaft Diameter Shaft 3 Distance Between Bearings on Shaft 3 Distance Between Bearing and Spur Gear 4	L3 LKJ LIK	240 150 90	mm mm	
Shaft Diameter Shaft 3 Distance Between Bearings on Shaft 3 Distance Between Bearing and Spur Gear 4 Tangential Force at Gear 4 (K)	L3 LKJ LIK FtK	240 150 90 368.366	mm mm	Mt/(dp4/2)
Shaft Diameter Shaft 3 Distance Between Bearings on Shaft 3 Distance Between Bearing and Spur Gear 4 Tangential Force at Gear 4 (K) Axial Force at Gear 14	L3 LKJ LIK FtK Fak	240 150 90 368.366 134.074	mm mm N	Ftk* tan20
Shaft Diameter Shaft 3 Distance Between Bearings on Shaft 3 Distance Between Bearing and Spur Gear 4 Tangential Force at Gear 4 (K) Axial Force at Gear 14 Resultant force at k	L3 LKJ LIK FtK Fak FrK	240 150 90 368.366 134.074 392.007	mm mm	· •
Shaft Diameter Shaft 3 Distance Between Bearings on Shaft 3 Distance Between Bearing and Spur Gear 4 Tangential Force at Gear 4 (K) Axial Force at Gear 14 Resultant force at k Weight of Gear 4	L3 LKJ LIK FtK Fak FrK Wg4	240 150 90 368.366 134.074 392.007 389.979	mm mm N N	Ftk* tan20
Shaft Diameter Shaft 3 Distance Between Bearings on Shaft 3 Distance Between Bearing and Spur Gear 4 Tangential Force at Gear 4 (K) Axial Force at Gear 14 Resultant force at k Weight of Gear 4 Total Force at Gear 4	L3 LKJ LIK FtK Fak FrK Wg4 Fk	240 150 90 368.366 134.074 392.007 389.979 781.986	mm mm N N N	Ftk* tan20 Ftk/ Cos20
Shaft Diameter Shaft 3 Distance Between Bearings on Shaft 3 Distance Between Bearing and Spur Gear 4 Tangential Force at Gear 4 (K) Axial Force at Gear 14 Resultant force at k Weight of Gear 4 Total Force at Gear 4 Reaction at J	L3 LKJ LIK FtK Fak FrK Wg4 Fk RJ	240 150 90 368.366 134.074 392.007 389.979 781.986 293.245	mm N N N N N	Ftk* tan20 Ftk/ Cos20 FK*LIK/L3
Shaft Diameter Shaft 3 Distance Between Bearings on Shaft 3 Distance Between Bearing and Spur Gear 4 Tangential Force at Gear 4 (K) Axial Force at Gear 14 Resultant force at k Weight of Gear 4 Total Force at Gear 4 Reaction at J Reaction at I	L3 LKJ LIK FtK Fak FrK Wg4 Fk RJ RI	240 150 90 368.366 134.074 392.007 389.979 781.986 293.245 488.742	mm N N N N N N	Ftk* tan20 Ftk/ Cos20 FK*LIK/L3 FK-RJ
Shaft Diameter Shaft 3 Distance Between Bearings on Shaft 3 Distance Between Bearing and Spur Gear 4 Tangential Force at Gear 4 (K) Axial Force at Gear 14 Resultant force at k Weight of Gear 4 Total Force at Gear 4 Reaction at J	L3 LKJ LIK FtK Fak FrK Wg4 Fk RJ	240 150 90 368.366 134.074 392.007 389.979 781.986 293.245	mm N N N N N	Ftk* tan20 Ftk/ Cos20 FK*LIK/L3
Shaft Diameter Shaft 3 Distance Between Bearings on Shaft 3 Distance Between Bearing and Spur Gear 4 Tangential Force at Gear 4 (K) Axial Force at Gear 14 Resultant force at k Weight of Gear 4 Total Force at Gear 4 Reaction at J Reaction at I Maximum Bending moment at K	L3 LKJ LIK FtK Fak FrK Wg4 Fk RJ RI MbK	240 150 90 368.366 134.074 392.007 389.979 781.986 293.245 488.742 43986.73551	mm N N N N N N N N N N N N N N N N N N	Ftk* tan20 Ftk/ Cos20 FK*LIK/L3 FK-RJ RI * LIK
Shaft Diameter Shaft 3 Distance Between Bearings on Shaft 3 Distance Between Bearing and Spur Gear 4 Tangential Force at Gear 4 (K) Axial Force at Gear 14 Resultant force at k Weight of Gear 4 Total Force at Gear 4 Reaction at J Reaction at I Maximum Bending moment at K Equivalent twisting moment	L3 LKJ LIK FtK Fak FrK Wg4 Fk RJ RI MbK	240 150 90 368.366 134.074 392.007 389.979 781.986 293.245 488.742 43986.73551 93540.65777	mm N N N N N N	Ftk* tan20 Ftk/ Cos20 FK*LIK/L3 FK-RJ RI * LIK sqrt((Kb*MbK)^2+(Kt*Mt)^2)
Shaft Diameter Shaft 3 Distance Between Bearings on Shaft 3 Distance Between Bearing and Spur Gear 4 Tangential Force at Gear 4 (K) Axial Force at Gear 14 Resultant force at k Weight of Gear 4 Total Force at Gear 4 Reaction at J Reaction at I Maximum Bending moment at K	L3 LKJ LIK FtK Fak FrK Wg4 Fk RJ RI MbK	240 150 90 368.366 134.074 392.007 389.979 781.986 293.245 488.742 43986.73551	mm N N N N N N N N N N N N N N N N N N	Ftk* tan20 Ftk/ Cos20 FK*LIK/L3 FK-RJ RI * LIK
Shaft Diameter Shaft 3 Distance Between Bearings on Shaft 3 Distance Between Bearing and Spur Gear 4 Tangential Force at Gear 4 (K) Axial Force at Gear 14 Resultant force at k Weight of Gear 4 Total Force at Gear 4 Reaction at J Reaction at I Maximum Bending moment at K Equivalent twisting moment Shaft 3 Diameter cube	L3 LKJ LIK FtK Fak FrK Wg4 Fk RJ RI MbK Te3 d3^3	240 150 90 368.366 134.074 392.007 389.979 781.986 293.245 488.742 43986.73551 93540.65777 11761.40482	mm mm N N N N N N N N N N N N N N N N N	Ftk* tan20 Ftk/ Cos20 FK*LIK/L3 FK-RJ RI * LIK sqrt((Kb*MbK)^2+(Kt*Mt)^2)
Shaft Diameter Shaft 3 Distance Between Bearings on Shaft 3 Distance Between Bearing and Spur Gear 4 Tangential Force at Gear 4 (K) Axial Force at Gear 14 Resultant force at k Weight of Gear 4 Total Force at Gear 4 Reaction at J Reaction at I Maximum Bending moment at K Equivalent twisting moment Shaft 3 Diameter Considering next std value for Shaft	L3 LKJ LIK FtK Fak FrK Wg4 Fk RJ RI MbK Te3 d3^3 d3	240 150 90 368.366 134.074 392.007 389.979 781.986 293.245 488.742 43986.73551 93540.65777 11761.40482 22.742 22.00	mm mm N N N N N N N N N mm n mm	Ftk* tan20 Ftk/ Cos20 FK*LIK/L3 FK-RJ RI * LIK sqrt((Kb*MbK)^2+(Kt*Mt)^2)
Shaft Diameter Shaft 3 Distance Between Bearings on Shaft 3 Distance Between Bearing and Spur Gear 4 Tangential Force at Gear 4 (K) Axial Force at Gear 14 Resultant force at k Weight of Gear 4 Total Force at Gear 4 Reaction at J Reaction at I Maximum Bending moment at K Equivalent twisting moment Shaft 3 Diameter cube Shaft 3 Diameter	L3 LKJ LIK FtK Fak FrK Wg4 Fk RJ RI MbK Te3 d3^3	240 150 90 368.366 134.074 392.007 389.979 781.986 293.245 488.742 43986.73551 93540.65777 11761.40482 22.742	mm mm N N N N N N N N N mm n mm	Ftk* tan20 Ftk/ Cos20 FK*LIK/L3 FK-RJ RI * LIK sqrt((Kb*MbK)^2+(Kt*Mt)^2)
Shaft Diameter Shaft 3 Distance Between Bearings on Shaft 3 Distance Between Bearing and Spur Gear 4 Tangential Force at Gear 4 (K) Axial Force at Gear 14 Resultant force at k Weight of Gear 4 Total Force at Gear 4 Reaction at J Reaction at I Maximum Bending moment at K Equivalent twisting moment Shaft 3 Diameter cube Shaft 3 Diameter Considering next std value for Shaft Dia	L3 LKJ LIK FtK Fak FrK Wg4 Fk RJ RI MbK Te3 d3^3 d3	240 150 90 368.366 134.074 392.007 389.979 781.986 293.245 488.742 43986.73551 93540.65777 11761.40482 22.742 22.00	mm mm N N N N N N N N mm n mm	Ftk* tan20 Ftk/ Cos20 FK*LIK/L3 FK-RJ RI * LIK sqrt((Kb*MbK)^2+(Kt*Mt)^2)
Shaft Diameter Shaft 3 Distance Between Bearings on Shaft 3 Distance Between Bearing and Spur Gear 4 Tangential Force at Gear 4 (K) Axial Force at Gear 14 Resultant force at k Weight of Gear 4 Total Force at Gear 4 Reaction at J Reaction at I Maximum Bending moment at K Equivalent twisting moment Shaft 3 Diameter cube Shaft 3 Diameter Considering next std value for Shaft Dia Bearing Selection	L3 LKJ LIK FtK Fak FrK Wg4 Fk RJ RI MbK Te3 d3^3 d3	240 150 90 368.366 134.074 392.007 389.979 781.986 293.245 488.742 43986.73551 93540.65777 11761.40482 22.742 22.00 30.00	mm mm N N N N N N N N mm mm mm	Ftk* tan20 Ftk/ Cos20 FK*LIK/L3 FK-RJ RI * LIK sqrt((Kb*MbK)^2+(Kt*Mt)^2)
Shaft Diameter Shaft 3 Distance Between Bearings on Shaft 3 Distance Between Bearing and Spur Gear 4 Tangential Force at Gear 4 (K) Axial Force at Gear 14 Resultant force at k Weight of Gear 4 Total Force at Gear 4 Reaction at J Reaction at I Maximum Bending moment at K Equivalent twisting moment Shaft 3 Diameter cube Shaft 3 Diameter Considering next std value for Shaft Dia	L3 LKJ LIK FtK Fak FrK Wg4 Fk RJ RI MbK Te3 d3^3 d3	240 150 90 368.366 134.074 392.007 389.979 781.986 293.245 488.742 43986.73551 93540.65777 11761.40482 22.742 22.00	mm mm N N N N N N N N mm n mm	Ftk* tan20 Ftk/ Cos20 FK*LIK/L3 FK-RJ RI * LIK sqrt((Kb*MbK)^2+(Kt*Mt)^2)

Load factor / Service Factor (Ks)		1.5		
Bearing ID		25	mm	
Bearing OD		47	mm	
Thickness		12	mm	
Static Load Rating	C01	6.55	KN	
Dynamic Load Rating	C1	11.9	KN	
Radial load at Bearing A	Fra	796.264	N	Ra
Axial Load at Bearing A	Faa	0	N	
RADIAL LOAD RATING FOR BEARING	X	1		
AXIAL LOAD RATING FOR	Λ	1		
BEARING	Y	1		
EQUIVALENT DYNAMIC				
BEARING LOAD	Pb	1194.396078		$(XF_r+YF_a)*Ks$
Bearing life in Revolutions	LRev	989.00	Millions	of revolutions

Figure 6: Drafted View of Gearbox

6. CONCLUSION

The objective was to customize CATIAV5 for design two stage spur gearbox with minimum user requirements (inputs). With the help of this customization gearbox is generated. Also the time required for generating part model (three dimensional model) of gearbox is reduced to few minutes. This part model can be used to draft different views of the gearbox which can directly be used for manufacturing processes. Thus, customization will increase productivity of the designer with increase in quality of design which in turn reduces lead time for design of gearbox.

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