



INTERNATIONAL JOURNAL OF ADVANCE RESEARCH, IDEAS AND INNOVATIONS IN TECHNOLOGY

ISSN: 2454-132X

Impact factor: 4.295

(Volume3, Issue3)

Available online at www.ijariit.com

Microstructural Characterisation of Thermal Spray Coatings on Stainless Steel AISI Ss-316 L

Hitesh Saini

RIET, Phagwara

M.Tech Research Scholar

hiteshvasudev@yahoo.in

Er. Pardeep Singh

Assistant Professor

RIET, Phagwara

Abstract: Thermal spray coating process is a surface modification technique in which a coating material like cermet's, metallic, ceramic and some other materials in form powder are feed into a torch or a gun, the powder inserted into torch will be melted by high temperature developed by a torch. Coating thickness can achieve by applying multiple layers of melted coated material. This paper aims at the study of microstructural characterisation of thermal spray single layer and multi-layer coatings. Coatings on the substrate were followed by Scanning electron microscopy to know the different phases present in the coated as well uncoated SS 316L. By seeing SEM result it's found that single layer coating is not done properly. As compared to SEM result of the single layer coated AISI 316 L multilayer SEM results is more accurate, there is no crack on the coating surface and there is much less porosity in the multilayer coated sample.

Keywords: SEM, Phases, Cracks.

I. INTRODUCTION

AISI316L is most commonly used steel in industries their application is Marines, pressure vessels, heat exchangers, valves, pumps pipelines, food related processing, medical equipment. AISI316L grade shows good resistance against corrosion under normal environments conditions like in normal seawater solutions containing 35g/l NaCl in distilled water. Generally, seawater is very often described as 3.5% NaCl solution however seawater is much more complex than just simple kitchen salt solution. The composition of seawater, temperature, movement in the tidal zone, salinity, oxygen concentration, and biological activity are etc differ from location to location and these are important parameters that effect the corrosion behaviours of stainless steel in seawater [1]. Stainless steel consists of various group and each one having different grade classify according to their chemical constituents [13]. The stainless steel having Fe and Cr 12 to 18 consider as ferritic steel such type of steel doesn't consist Ni. Ferritic steel consists of small amount of non-heat treatable carbon but shows excellent corrosion resistance to and oxidation as compared to martensitic. Martensitic stainless steel consists of carbon 0.19 to 1.1% and Cr 11 to 17% [15]. The heat treatment can be done on such materials and their corrosion resistance properties are not too good as compare to other materials having the same amount of Cr and other alloy composition. Duplex stainless steel consists of copper, iron, nickel (4-7%), chromium (18-26%), and molybdenum (0-4%). It showed the microstructure of both austenitic and ferritic thus provide the properties of corrosion resistance and have greater strength [11]. Austenitic stainless steel consists of Fe, Cr 15% to 25% and Ni 5 % to 11 properties can be improved further by adding molybdenum added as per requirement. It exhibits superior corrosion resistance properties as compared to Ferritic and Martensitic, Example of austenitic stainless steel is AISI 316L. Although stainless steel is having better as compare to corrosion resistance than any other carbon or alloy steel, in some circumstance, it can corrode [9]. It's stainless steel, not stain-impossible steel. In normal water based environment and atmospheric condition stainless steel will not corrode, but in the more aggressive condition the basic type of stainless steel corrodes and more highly stainless steel is required [7].

II. EXPERIMENTAL ANALYSIS

2.1 Specimens preparation for SEM test

Initially three specimens were cut out from AISI 316L sheet of square dimension having length and breadth 15 mm. One specimens is single layer coated with Inconel 718 using D-gun thermal spray method and second specimens is coated double layer using the same method and third specimens is remain pure AISI 316L in square form without any coating.

2.2 Scanning Electron Microscope (SEM) test

Scanning electron microscopes electron microscopy which produced fine images of samples by scanning the sample electron beam. Focused beam electron interacts with atoms in the specimen producing various signals which contain information about the surface of the sample and different chemical composition. Raster scan pattern is generally used for scanning by the electron and beam position is combined with detected to generate an image. Raster scanning is a rectangular pattern of image capturing and reconstructing in television. SEM produces better resolution quality of sample images than 1 nanometre. The entire specimen must have a standard size such that it takes place in the sample holder. SEM produces better resolution than the optical microscope. Specimens can be checked in low vacuum, high vacuum, in wet condition and a wide range of cryogenic or high temperature.

Initially, the specimen surface was cleaned properly then an electron beam having energy high energy is focused on the sample this beam is having very narrower dia. From final lens, the electron beam is deflected two axes such that it can that it can scan a rectangular area over the surface.

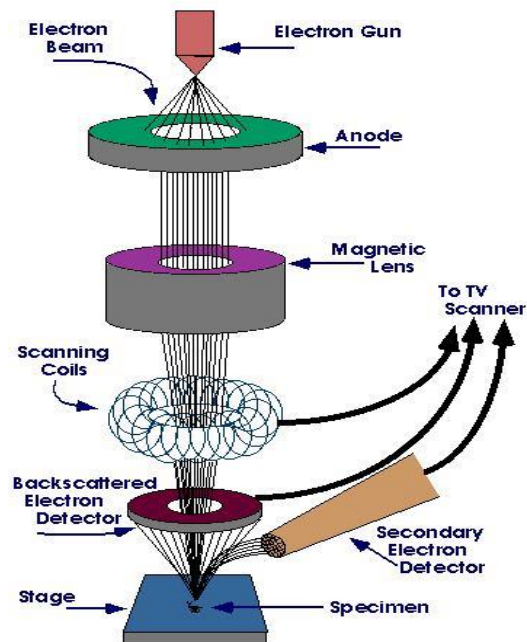


Fig.3.11 Scanning Electron Microscope Diagram

III. RESULTS

3.1 SEM TEST

SEM test will give the brief discussion about the surface characteristic of specimens before and after the corrosion test. With the help of SEM test surface characteristics like porosity, wears, un-melted powder particles, cracks, and pits etc. are study briefly.

SEM test is used to find out the reason for different surface properties of the similar sample, like if two same coated samples and if the surface of one coated sample corrodes more rapidly as compared to another than by using SEM test reason for this is to find out.

Below figure3.1show the SEM result of single layer Inconel 718 coated stainless steel sample at magnification of 2000mg. Different surface properties like cracks, porosity, and semi-melted coating powder are noted in Figure. By seeing SEM result it's found that single layer coating is not done properly. This is why data collected from corrosion resistance showed no weight loss different between stainless steel and coated stainless steel. Because of cracks corrosion resistance properties of coated stainless steel are affected in a negative manner, both coated stainless steel and uncoated stainless steel loss same 0.0002 gram of weight after taking out the specimens from stagnant seawater.

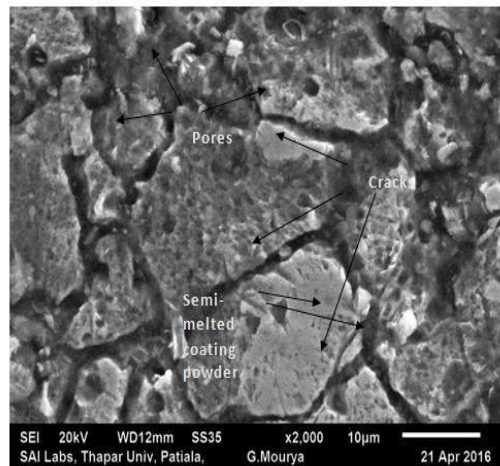


Figure 3.1 SEM result of single layer coated sample before corrosion test

Figure 3.2 showed the SEM result of multilayer coated AISI 316L with Inconel 718 powder. Details description of the surface structure of multilayer coated AISI 316L are shown in the figure. As compared to SEM result of the single layer coated AISI 316 L multilayer SEM results is more accurate, there is no crack on the coating surface and there is much less porosity in the multilayer coated sample. Because of very less crack in coating surface and dense coating corrosion resistance properties of multilayer sample is much greater than single layer coated sample and uncoated stainless steel sample. Bonding between the coated powders are good and it's shown by dense regions.

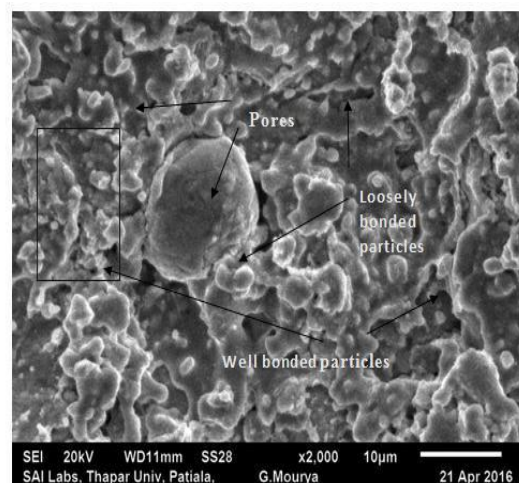


Figure 3.2 SEM result of multilayer coated sample before corrosion test

Figure 3.3 showed the SEM result of stainless steel AISI 316L at 2000 magnification after corrosion test in stagnant seawater. By observing the SEM result it is noted that stainless steel surface contains lots of up and downs, this is because of materials removed from that place some pits are also observed in the figure. Materials removals and pitting formation occurred because specimen is dipped in stagnant seawater for 96 hours

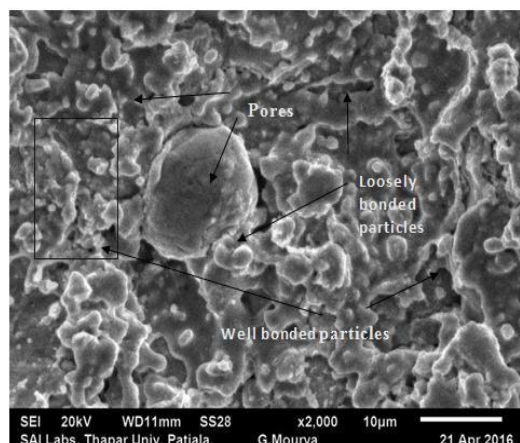


Figure 3.3 SEM result of multilayer coated sample before corrosion test

Figure 3.4 showed SEM result of the single layer coated stainless steel AISI 316L at 2000 magnification after corrosion test in stagnant seawater for 96 hours. Particles removed and pits are clearly seen in the figure. Comparing figure 11 and 12 in both the figure, weight loss or particles removed are almost same but pits are generally more in figure 11 i.e. in uncoated stainless steel sample pits are more.

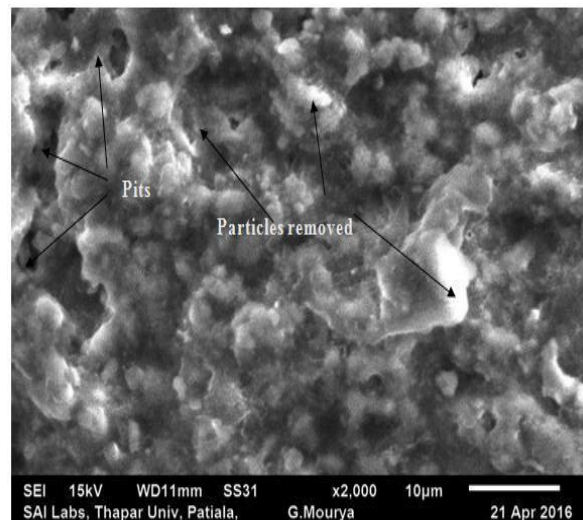


Figure 3.4 SEM result of single layer coated AISI 316L after corrosion test

Figure 3.4 showed SEM result of multilayer coated stainless steel AISI 316L with Inconel 718 powder after conducting corrosion test on the specimen for 96 hours. SEM result was recorded at 500 magnifications. From the figure it is noticed that particles removed are very less and pitting observed is also very less as compared to another specimen.

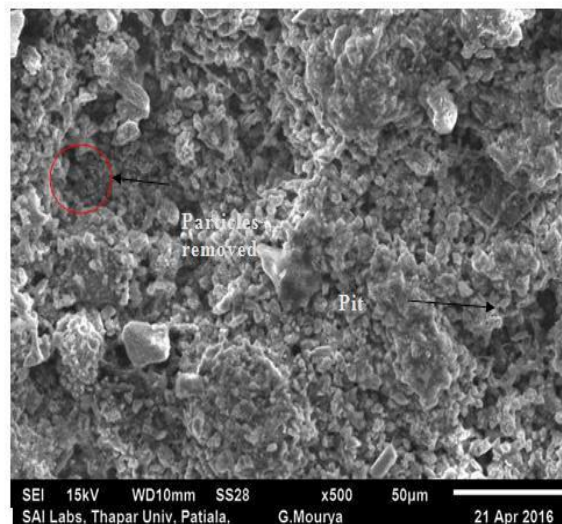


Figure 3.5 SEM result of multilayer coated AISI 316L after corrosion test

Comparing all the three specimens of after corrosion test it was found that particles removed is same in uncoated stainless steel and a single layer coated stainless steel but in the case of multilayer coated stainless steel particles removed are very less as compared to both specimens. Number of pits are formed on uncoated stainless steel as compared to single layer coated specimen and multilayer coated specimens.

CONCLUSIONS

SEM test was conducted in this paper which help in studying the different characteristic of coating and uncoating specimens it also helps in the study the corrosion behaviours of uncoated stainless steel AISI 316L and coated AISI 316L.

REFERENCES

1. Jin, Z. H., Ge, H. H., Lin, W. W., Zong, Y. W., Liu, S. J., & Shi, J. M. (2014). Corrosion behaviour of 316L stainless steel and anti-corrosion materials in a high acidified chloride solution. *Applied Surface Science*, 322, 47–56. doi:10.1016/j.apsusc.2014.09.205

2. Ramkumar, K. D., Dev, S., Saxena, V., Choudhary, A., Arivazhagan, N., & Narayanan, S. (2015). Effect of flux addition on the microstructure and tensile strength of dissimilar weldments involving Inconel 718 and AISI 416. *JMADE*, 87, 663–674. doi:10.1016/j.matdes.2015.08.075
3. Gill, A. S., Telang, A., & Vasudevan, V. K. (2015). Journal of Materials Processing Technology Characteristics of surface layers formed on Inconel 718 by laser shock peening with and without a protective coating. *Journal of Materials Processing Tech.*, 225, 463–472. doi:10.1016/j.jmatprotec.2015.06.026
4. Kawakita, J., Kuroda, S., Fukushima, T., & Kodama, T. (2005). Improvement of Corrosion Resistance of High-Velocity Oxyfuel-Sprayed Stainless Steel, *14*(June), 224–230. doi:10.1361/10599630523782
5. Kayali, Y., & Büyüksa, A. (2013). Corrosion and Wear Behaviors of Boronized AISI 316L Stainless Steel, *19*(5), 1053–1061. doi:10.1007/s12540-013-5019-x
6. Zeng, C. L., Lin, H. C., & Cao, C. N. (2001). Electrochemical corrosion behaviour of type 316 stainless steel in acid media containing fluoride ions, *36*(3), 179–183.
7. Mann, B. S., & Arya, V. (2003). HVOF coating and surface treatment for enhancing droplet erosion resistance of steam turbine blades, *254*, 652–667. [http://doi.org/10.1016/S0043-1648\(03\)00253-9](http://doi.org/10.1016/S0043-1648(03)00253-9)
8. Sheng, X., Pehkonen, S. O., & Ting, Y. (2012). Biocorrosion of stainless steel 316 in seawater: inhibition using anazole type derivative, *47*(5), 388–394. <http://doi.org/10.1179/1743278212Y.0000000014>
9. Sun, B., Fukunuma, H., & Ohno, N. (2014). Surface & Coatings Technology Study on stainless steel 316L coatings sprayed by a novel high-pressure HVOF. *Surface & Coatings Technology*, 239, 58–64. <http://doi.org/10.1016/j.surfcoat.2013.11.018>
10. Totemeier, T. C. (2005). Effect of High-Velocity Oxygen-Fuel Thermal Spraying on the Physical and Mechanical Properties of Type 316 Stainless Steel, *14*(September), 369–372. <http://doi.org/10.1361/105996305X59440>
11. Wv, H. (1958). Versatile Corrosion Resistance of INCONEL Alloy 625 in Various Aqueous and Chemical Processing Environments, 663–680.
12. Yilbas, B. S., & Khalid, M. (2003). Corrosion Behavior of HVOF Coated Sheets, *12*(December), 572–575.
13. Envelhecimento, T. T. D. E. (2014). “Analysis of pitting corrosion on an Inconel 718 alloy submitted to aging heat treatment”, 189–194.
14. Khan F. F., G. Bae, K. Kang, H. Na, J. Kim, T. Jeong, and C. Lee, (2011) Evaluation of Die- Soldering and Erosion Resistance of High-Velocity Oxy-Fuel Sprayed MoB-Based Cermet Coatings, *Journal of Thermal Spray Technology* 20(5) 1022-1034.
15. Knuuttila J., P. Sorsa, T. Mäntylä, J. Knuuttila and P. Sorsa, (1999) Sealing of thermal spray coatings by impregnation, *Journal of Thermal Spray Technology* 8(2) 249-25.
16. Lebedev A. S. and S. V. Kostennikov, (2008) Trends in Increasing Gas-Turbine Units Efficiency, *Thermal Engineering* 55(6) 461-468.
17. Lee S.-H., N. J. Themelis and M. J. Castaldi, (2007) High-Temperature Corrosion in Waste-to- Energy Boilers, *Journal of Thermal Spray Technology* 16(1) 104-110.
18. Leivo E., T. Wilenius, T. Kinos, P. Vuoristo, T. Mäntylä, (2004) Properties of thermally sprayed fluoropolymer PVDF, ECTFE, PFA and FEP coatings, *Progress in Organic Coatings* 49 69–73.
19. Leivo E.M., M.S. Vippola, P.P.A.Sorsa, P.M. & Vuoristo, and T.A.Mäntylä, (1997) Wear and Corrosion Properties of Plasma Sprayed Al₂O₃ and Cr₂O₃ Coatings Sealed by Aluminum Phosphates, *Journal of Thermal Spray Technology* 6(2) 205-210.
20. Lenling W.J., M.F. Smith and J.A. Henfling, (1991) Beneficial effects of austempering posttreatment on tungsten carbide based wear coatings, in *Thermal Spray Research and Applications* (ed.) T.F. Bernecki (pub.) ASM Int. Materials Park, OH, USA 227-232.
21. Li L., N. Hitchman, and J. Knapp, (2010) Failure of Thermal Barrier Coatings Subjected to CMAS Attack, *Journal of Thermal Spray Technology* 19(1-2) 148-155 .
22. Lima R.S. and B.R. Marple, (2007) Thermal Spray Coatings Engineered from Nanostructured Ceramic Agglomerated Powders for Structural, Thermal Barrier and Biomedical Applications: A Review, *Journal of Thermal Spray Technology* 16(1) 40-63.
23. Lima R.S. and B.R. Marple, (2005) Superior Performance of High-Velocity Oxyfuel-Sprayed Nanostructured TiO₂ in Comparison to Air Plasma-Sprayed Conventional Al₂O₃- 13TiO₂, *Journal of Thermal Spray Technology* 14(3) 397-404.
24. Lin L. and K.Han, (1998) Optimization of surface properties by flame spray coating and boriding, *Surface and Coatings Technology* 106 100–105.
25. Liu Z., J. Cabrero, S. Niang, Z.Y. Al-Taha, (2007) Improving corrosion and wear performance of HVOF-sprayed Inconel 625 and WC-Inconel 625 coatings by high power diode laser treatments, *Surface & Coatings Technology* 201, 7149–7158 .
26. Ma X., A. Matthews, (2009) Evaluation of abrasible seal coating mechanical properties, *Wear* 267, 1501–1510.
27. Maranhão O., D. Rodrigues, M. Boccalini, and A. Sinatoro, (2009) Bond Strength of Multicomponent White Cast Iron Coatings Applied by HVOF Thermal Spray Process, *Journal of Thermal Spray Technology* 18(4) 708-713 .
28. Markocsan N., P. Nylén, J. Wigren, X.-H. Li, and A. Tricoire, (2009) Effect of Thermal Aging on Microstructure and Functional Properties of Zirconia-Base Thermal Barrier Coatings, *Journal of Thermal Spray Technology* 18(2) 201-208.