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Mathematical Modeling of Soft Switched Single Stage Multistring Inverter with Multi-Rated ETT Photovoltaic Modules

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Abstract—This paper presents the preliminary study of modeling of single stage multi string inverter with multi rated easy to tune model of photo voltaic modules. As the name represents, the Multi string topology is capable of handling more number of PV strings with different orientations and varied irradiation levels. This multi string inverter is able to harvest the maximum possible power from each string independently, while they may be at different operating temperatures. In this paper a multi string inverter with two different easy-to-tune (ETT) PV modules using MATLAB/SIMULINK has been implemented and detailed analysis is carried out with and without filters. Total harmonic distortion of output is also evaluated.

Keywords—Multi string inverter, easy to tune (ETT) photo voltaic module, total harmonic distortion (THD), filter.

I. INTRODUCTION

Because of rapid depletion of conventional energy resources electrical power system integration with renewable energy resources is made prominent in present research areas. The solar energy may be one of the most alternative energy resource in future. Photovoltaic (PV) inverter is the heart of the solar energy conversion systems since they collect the maximum possible power from PV cells for delivery to a utility grid or stand-alone loads. Different configurations of PV inverters have been proposed, which are mainly categorized as centralized, string, multistring, and microinverter. In the centralized configuration, a number of PV modules are connected in series (called a PV string), and multiple PV strings are connected to a main inverter using diodes. Although the large, centralized inverter offers economies of scale, this approach offers poor energy harvesting due to one centralized maximum power point (MPP) tracker for the whole system; partial shading or any mismatch between the PV modules causes a substantial drop in the generated power output. The microinverter solution employs the opposite approach by using a small inverter for individual MPP tracking of each PV module, maximizing possible energy harvesting. Therefore, reducing or even losing the output of a single module due to partial shading or an inverter failure has a minimal impact on the overall system performance. However, the main drawback of the microinverter concept is a higher initial equipment cost per peak watt. This increased cost is due to the use of an inverter for each panel with much of the functionality of a centralized inverter. In smaller PV systems, such as residential applications, the inverter price has less effect on the overall cost, and therefore, microinverters are the preferred solution. As the price of microinverters comes down, this technology will be more attractive in other applications. String technology is another configuration for PV systems, where a string of PV modules is connected to a single inverter integrated with an MPP tracker. Therefore, the string inverter can avoid most of the weaknesses of the centralized configuration. Nonetheless, the string technology has a power limit due to a limited number of series connections. The multistring solution is an enhanced version of the string topology and ensures optimum energy harvesting and cost.

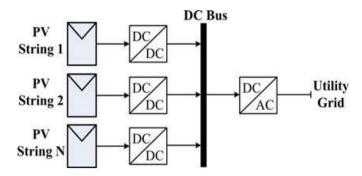


Fig.1 conventional configuration

In its conventional configuration, several strings are interfaced with their own MPP-tracked dc-dc converter to a common inverter as shown in Fig. 1. The multistring approach allows the integration of strings with different features with respect to the manufacturing technology, geographic orientation, and number of modules per string. It also enables the enhanced operation of the PV systems in partial shading conditions when the PV strings are at different irradiance levels and operating temperatures . The conventional multistring PV topology has the disadvantage of poor conversion efficiency because of two stages of power conversion and the use of several bulky limited-lifetime electrolytic capacitors in the main dc-link.

A soft switched single-stage multistring PV inverter with multi rated easy to tune photo voltaic modules has been presented in this paper. Similar to the conventional multistring topology, the proposed inverter can handle an arbitrary number of PV strings with different electrical parameters and working conditions while obtaining the maximum possible power from each string independently. However, the proposed topology has a single stage of soft switched power conversion with no electrolytic capacitor in the link. Therefore, this converter is expected to have an improved efficiency, high power density, and enhanced reliability. The new inverter has an HFAC link, so a small-sized high-frequency (HF) transformer has been employed to achieve galvanic isolation.

II. EASY TO TUNE PV MODULE

Photovoltaic (PV) array which is composed of modules is considered as the fundamental power conversion unit of a PV generator system. The PV array has nonlinear characteristics and it is quite expensive and takes much time to get the operating curves of PV array under varying operating conditions. In order to overcome these obstacles, common and simple models of solar panel have been developed and integrated to many engineering software including Matlab/Simulink. However, these models are not adequate for application involving hybrid energy system since they need a flexible tuning of some parameters in the system and not easily understandable for readers to use by themselves. DS-100M solar panel is used as reference model. The operation characteristics of PV array are also investigated at a wide range of operating conditions and physical parameters.

Mathematical modeling of PV module is being continuously updated to enable researchers to have a better understanding of its working. The models differ depending on the types of software researchers used such as C programming, Excel, Matlab, Simulink or the toolboxes they developed. A function in Matlab environment has been developed to calculate the current output from data of voltage, solar irradiation and temperature in the study of (Walker 2001) and (Gonzalez-Longatt 2005). Here, the effect of temperature, solar irradiation, and diode quality factor and series resistance is evaluated. A difficulty of this method is to require readers programming skills so it is not easy to follow. Another method which is the combination between Matlab m-file and C-language programming is even more difficult to clarify (Gow and Manning 1999). Among other authors, a proposed model is based on solar cell and array's mathematical equations and built with common blocks in Simulink environment in (Salmi et al. 2012), (Panwar and Saini 2012), (Savita Nema and Agnihotri 2010), and (Sudeepika and Khan 2014). In these studies, the effect of environmental conditions (solar insolation and temperature), and physical parameters (diode's quality factor, series resistance Rs, shuntresistance Rsh, and saturation current, etc.) is investigated. One disadvantage of these papers is lack of presenting simulation procedure so it causes difficulties for readers to follow and simulate by themselves later. This disadvantage is filled in by (Jena et al. 2014), (Pandiarajan and Muthu 2011). A step-by-step procedure for simulating PV module with subsystem blocks with user-friendly icons and dialog in the same approach with Tarak Salmi and Savita Nema is developed by Jena, Pandiarajan and Muthu et al. However, the biggest gap of the studies mentioned above is shortage of considering the effect of partially shading condition on solar PV panel's operation. In other researches, authors used empirical data and Lookup Table or Curve Fitting Tool (CFtool) to build P-V and I-V characteristics of solar module (Banu and Istrate 2012). The disadvantage of this method is that it is quite challenging or even unable to collect sufficient data if no experimental system be available so that modeling curves cannot be built and modeled. From the work of (Ibbini et al. 2014) and (Venkateswarlu and Raju 2013), a solar cell block which has already been built in Simscape/Simulink environment is employed. With this block, the input parameters such as short circuit current, open circuit voltage, etc. is provided by manufacturers. The negative point of this approach is that some parameters including saturation current, temperature, and so on cannot be evaluated. Solar model developed with Tag tools in Simulink environment is recorded in the research of (Varshney and Tariq 2014), (Mohammed 2011), etc. In these papers, only two aspects (solar irradiation and temperature) are investigated without providing step-by-step simulation procedure. In overall, although having advantages and disadvantages, different methods have similar gaps as follows:

- •• previous models are not totally sufficient to study all parameters which can significantly affect to I–V and P–V characteristics of solar PV array, including physical parameters such as saturation current, ideality factor, series and shunt resistance, etc. and environmental working conditions (solar insolation, temperature and especially shading effect).
- •• The proposed model shows strength in investigating all parameters' influence on solar PV array's operation. In addition, a unique step by-step modeling procedure shown allows readers to follow and simulate by themselves to do research. The equivalent circuit of a PV cell is shown in Fig. 1. The current source Iph represents the cell photocurrent. Rsh and Rs are the intrinsic shunt and series resistances of the cell, respectively. Usually the value of Rsh is very large and that of Rs is very small, hence they may be neglected to simplify the analysis (Pandiarajan and Muthu 2011). Practically, PV cells are grouped in larger units called PV modules and these modules are connected in series or parallel to create PV arrays which are used to generate electricity in PV generation systems. The equivalent circuit for PV array is shown in Fig. 2. The voltage–current characteristic equation of a solar cell is provided as (Tu and Su 2008; Salmi et al. 2012):

Pv cell output voltage is given by

$$V_c = \frac{AkT_c}{q} \ln \left(\frac{I_{ph} + I_0 - I_c}{I_0} \right) - R_s I_c$$

Module photo-current Iph:

 $I_{ph} = [I_{sc} + K_i(T - 298)] \times I_r/1000$

Here, Iph: photo-current (A); Isc: short circuit current (A);

Ki: short-circuit current of cell at 25 °C and 1000 W/m²;

T: operating temperature (K); Ir: solar irradiation (W/m²). Module reverse saturation current Irs:

 $I_{rs} = I_{sc}/[exp(qV_{oc}/N_sknT) - 1]$

Here, q: electron charge, = 1.6×10^{-19} C;

Voc: open circuit voltage (V);

Ns: number of cells connected in series;

n: the ideality factor of the diode;

k: Boltzmann's constant = 1.3805×10^{-23} J/K.

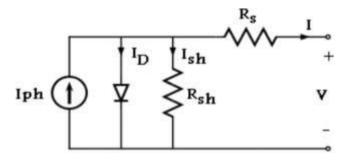


Fig. 2 PV cell equivalent circuit (Salmi et al. 2012)

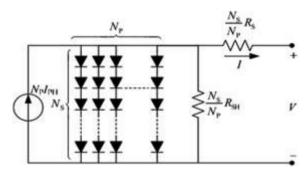


Fig. 3 Equivalent circuit of solar array (Tu and Su 2008)

The module saturation current IO varies with the cell temperature, which is given by:

$$I_0 = I_{rs} \left[\frac{T}{T_r} \right]^3 \exp \left[\frac{q \times E_{g0}}{nk} \left(\frac{1}{T} - \frac{1}{T_r} \right) \right]$$

Here, T_r : nominal temperature = 298.15 K;

 E_{g0} : band gap energy of the semiconductor, = 1.1 eV;

The current output of PV module is:

$$I = N_P \times I_{ph} - N_P \times I_0$$

$$\times \left[\exp\left(\frac{V/N_S + I \times R_s/N_P}{n \times V_t}\right) - 1 \right] - I_{sh}$$

With

$$V_t = \frac{k \times T}{q}$$

And

$$I_{sh} = \frac{V \times N_P/N_S + I \times R_S}{R_{sh}}$$

Here: Np: number of PV modules connected in parallel;

Rs: series resistance (Ω); Rsh: shunt resistance (Ω);

Vt: diode thermal voltage (V).

Reference model:

The 100 W solar power modules is taken as the reference module for simulation and the detailed parameters of module is given in Table below

Electrical characteristics data of DS-100 M PV Module:

The electrical specifications are under test conditions of irradiance of 1 kW/m², spectrum of 1.5 air masses and cell temperature of 25 °C

DS-100M Name 100 W Rated power (Vmp) Voltage at maximum power (Vmp) 18 V Current at maximum power (Imp) 5.55 A Open circuit voltage (VOC) 21.6 V Short circuit current (ISC) 6.11 A Total number of cells in series (NS) 36 Total number of cells in parallel (NP) 1 1000 V Maximum system voltage

Range of operation temperature -40 °C to 80 °C

A mathematical model of PV array including fundamental components of diode, current source, series resistor and parallel resistor is modeled with Tags in Simulink

Environment(http://mathwork.com). The simulation of solar module is based on equations given in the section above.

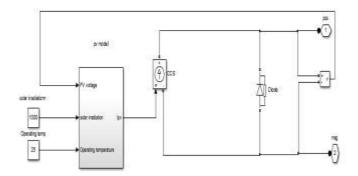


Fig.4 Solar subsystem Simulink design

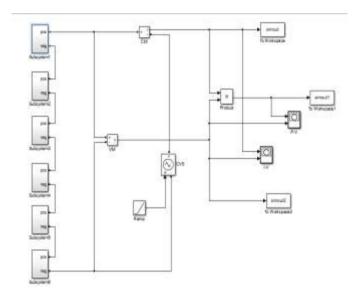


Fig. 5 Solar module Simulink design

III. SOFT SWITCHED MULTI STRING INVERTER

The soft-switched multistring PV inverter with multi-rated PV source is shown in Fig. 4. The number of the input PV strings as well as their characteristics, operating voltages, and power levels is completely random. The proposed inverter can individually collect the maximum possible power of each string regardless of its location, orientation, irradiation level, or operating temperature. A capacitor is placed on primary side of the transformer for soft switching and to behave as passive snubbers as well. In this way, they provide paths for the leakage inductance currents of the transformer when the switches are turned OFF and avoid voltage spikes.

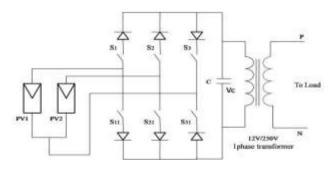


Fig.6 proposed soft switched multi string inverter

The converter needs to have two reverse-blocking switches for each PV string in addition to two more reverse-blocking switches for the return leg. A reverse-blocking switch can be realized by a conventional IGBT or MOSFET in series with a diode. The newly available individual reverse-blocking switches can also be employed with the advantage of lower total on-state voltage.

A. Control Strategy

The control strategy of the proposed multistring PV inverter is shown in Fig. 5. This scheme can be easily extended to a higher number of PV strings. Here two ETT PV panels are connected to the single stage multistring inverter. The driver circuit provides the gate signals to the switches in accordance with the control signals from the control circuit and also it isolates the gate signals from power signals. The control circuit provides six digital output control signals for six reverse blocking switches.

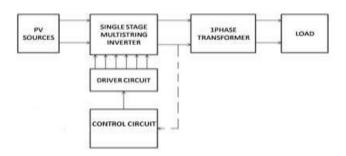


Fig. 7 Block diagram

Control circuit generates control signals according to the required output. A single phase 50Hz 12V/230V transformer is connected at the output of proposed multistring inverter to provide single phase 50Hz, 230V AC output. The output of the inverter is captured to calculate the Total Harmonic Distortion (THD).

B. Switching Algorithm of the Proposed Converter

The operation of the proposed soft-switched multistring inverter consists of several modes in each cycle depending on the number of PV panels connected. The switching flowchart of the converter is shown in Figure 6.Figures 7&8 shows the typical operating modes and link cycle of the proposed PV inverter in the two-string case. The described switching algorithm can be extended to higher number of input solar PV panels.

The entire 50Hz operating cycle can be divided into six modes with time period of 0.0033 seconds each. Total time period of cycle is 0.02 seconds.

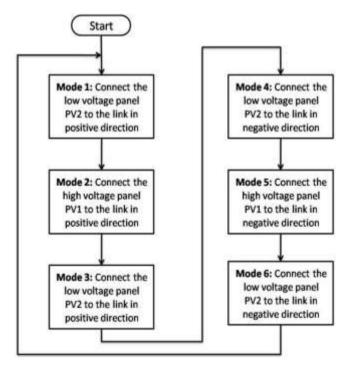


Fig. 8 Control flow chart

Mode 1 [see Fig. 9(a)]: Two PV-side switches (S₂ and S₃₁) are turned ON to connect the PV string with the lower instantaneous voltage to the inverter in the positive direction. This mode runs until 0.0033 seconds. Subsequently, the switches are turned OFF. In figures 5 and 6, it is assumed that PV1 voltage is higher than PV2 voltage. Therefore, PV2 is connected to the link in mode 1.

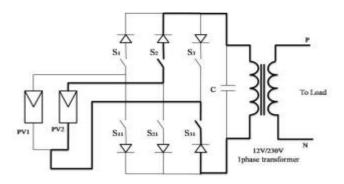


Fig. 9(a) Mode-1

Mode 2[see Fig. 9(b)]: The switches (S₁ and S₃₁) are turned ON to connect the PV string with the higher instantaneous voltage ie PV1 to the inverter in the positive direction. The switches are turned OFF after 0.0066 seconds.

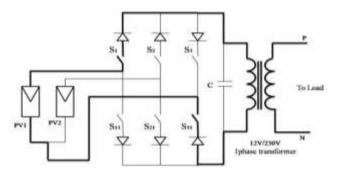


Fig. 9(b) Mode-2

Mode 3 [see Fig. 9(c)]: For obtaining a sinusoidal waveform at the output, the PV panel with lower instantaneous voltage is again connected to the inverter in positive direction. The PV-side switches (S2 and S31) are again turned ON. These switches are turned OFF after 0.01 seconds. The positive half cycle of the output waveform is completed after Mode 3. The described sequence of the PV string is important and should be followed flawlessly to operate the converter properly. If, for instance, the highest PV voltage is mistakenly connected to the link in mode 1, output waveform will be distorted.

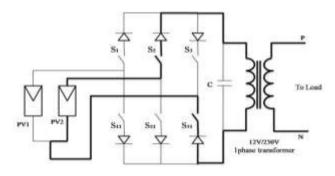


Fig. 9(c) Mode-3

Mode 4 [see Fig. 9(d)]: The negative half cycle starts with connecting the PV string with the lower instantaneous voltage ie PV2 to the inverter in the negative direction. Switches (S₂₁ and S₃) are turned ON to connect the PV string to the inverter. This mode runs until 0.0133 seconds and subsequently, the switches are turned OFF.

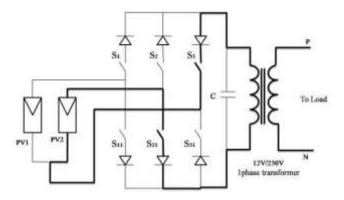


Fig. 9(d) Mode-4

Mode 5 [see Fig. 9(e)]: The switches (S₁₁ and S₃) are turned ON to connect the PV string with the higher instantaneous voltage ie PV1 to the HFAC link in the negative direction. The switches are turned OFF after 0.0166 seconds.

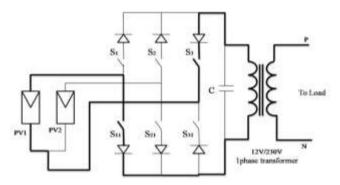


Fig. 9(e) Mode-5

Mode 6 [see Fig. 9(f)]: The switches (S₂₁ and S₃) are again turned ON to connect the PV string with the lower instantaneous voltage i.e., PV2 to the inverter in the negative direction. The switches are turned OFF after 0.02 seconds to complete the entire operating cycle.

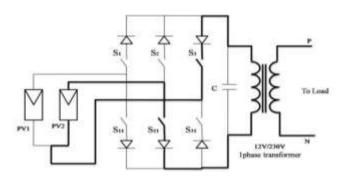


Fig. 9(f) Mode-6

A capacitor is connected across the output of the multistring inverter. Due to the existence of the capacitor, the link voltage 'Vc' changes slowly while the switches are turned OFF at the end of each mode. Consequently, the switch voltages change slowly at their turn-off. This provides a soft switching operation to the inverter reducing the switching losses and also functions as a filter.

A single phase two winding transformer is connected to step up the output voltage of multistring inverter to get the required level. The switching sequence of the reverse blocking switches is shown in the figure 6. The switch S₃₁ conducts for first half cycle for the flow of PV panel current in positive direction and switch S₃ conducts for the flow of PV panel current in negative direction. A 50Hz, 320V peak alternating voltage waveform is obtained at the output. A filter circuit is provided in the main circuit shown below to get voltage output with low total harmonic distortion (THD). Harmonic analysis of multi string inverter with and without filter is carried out

IV. SIMULATION RESULTS

The single stage multistring inverter was simulated using MATLAB/SIMULINK tool. The PV cell was designed and simulated with the help of its equivalent circuit shown in figures 2 & 3. Temperature and irradiation were considered as the changing parameters to change the output of the solar cell. Two PV cells of 12V and 24V were taken as input for the multistring configuration as per Figure 4. The switching circuit consists of reverse blocking switches using IGBTs and diodes which are taken from Simulink library. A two winding 12V/230V, 50Hz linear transformer is used to connect the inverter to the load side. Resistive load was considered for the simulation and the switching sequence were provided according to the operation described above. A 50Hz, 20V peak voltage waveform was obtained at inverter output. A 50Hz, 320V peak voltage waveform was obtained at secondary of transformer. The simulation diagram of multistring inverter with and without filter is shown in figure 10 and the output waveforms are shown in figure 11.

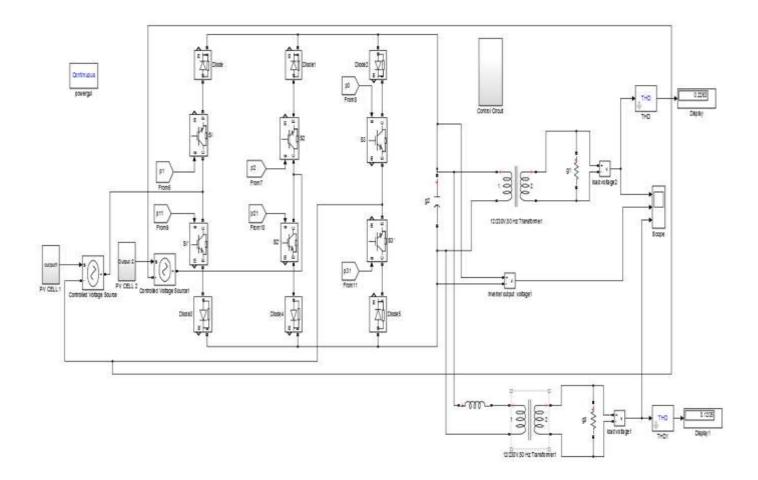


Fig. 10 Simulink design of proposed model

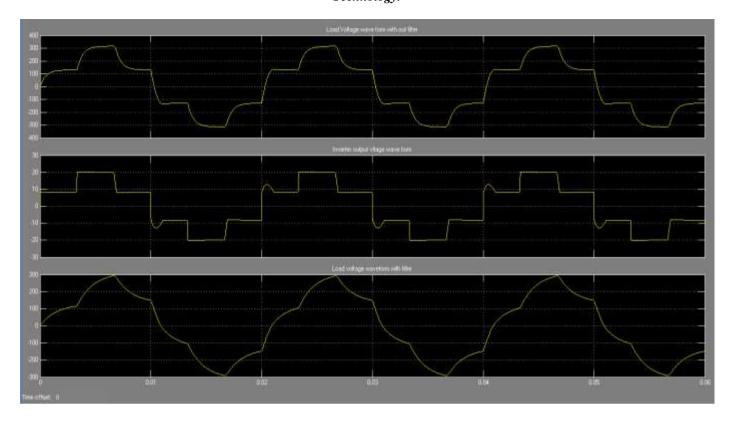


Fig. 11 Output voltage waveforms of load and inverter

CONCLUSION

A single stage soft-switched multistring inverter for PV systems was simulated using MATLAB/SIMULINK tool. This multi-rated source inverter can have an arbitrary number of PV strings and is able to obtain the maximum possible power of each string independently. The PV strings can be of different electrical parameters and working conditions. Simulated digital gate pulses are provided to the switches by control circuit. A single phase 50Hz transformer is responsible for boosting the voltage to required output level. Small ac capacitors on primary side of the transformer realize soft-switching operation. They also behave as passive snubbers to avoid voltage spikes. The control scheme and the switching algorithm of the proposed inverter were described. The output of inverter is also read to measure the THD using Matlab FFT analysis. THD of the output waveform was reduced to 12.83% using filter circuits.

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